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(71)出願人 000001247

光洋精工株式会社

大阪府大阪市中央区南船場3丁目5番8号

(72)発明者 高橋 裕

大阪府大阪市中央区南船場三丁目5番8号

光洋精工株式会社内

(74)代理人 弁理士 青山 葵 (外1名)

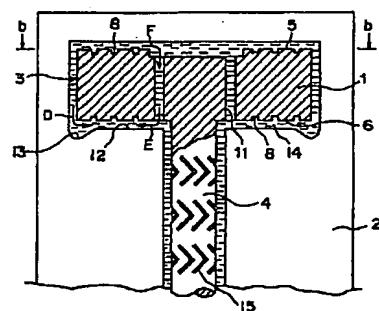
(54)【発明の名称】 密閉形スラスト動圧軸受

(57)【要約】

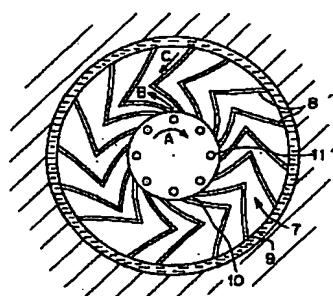
【課題】 起動時に軸方向に支持する動圧を十分に発生することができ、端面等を損傷することができない密閉形スラスト動圧軸受を提供する。

【解決手段】 ハウジング2内に回転体3のフランジ1を密封状態で収納する。上記フランジ1の上下両端面5,6にV字形の動圧発生溝8を設けると共に、上記フランジ1には動圧発生溝8より径方向内側に軸方向に貫通する複数の孔11を設ける。また、上記孔11の断面積の総和が環状領域7面積の少なくとも1/30とする。さらに、上記フランジ1の下側の端面6に対向するハウジング2の受面12には油溜まり13を設ける。

(a)



(b)



【特許請求の範囲】

【請求項1】 軸体とこの軸体の一端に設けられたフランジとから成る回転体と、この回転体のフランジを密閉状態で収納するハウジングとを備え、上記フランジの端面またはこの端面に対向する上記ハウジングの受面に動圧発生溝が設けられている密閉形スラスト動圧軸受において、

上記フランジは、上記動圧発生溝が設けられた環状領域よりも径方向内側に軸方向に貫通する少なくとも1つの孔を備えていることを特徴とする密閉形スラスト動圧軸受。

【請求項2】 請求項1に記載の密閉形スラスト動圧軸受において、上記孔の断面積の総和が上記環状領域の少なくとも1/30であることを特徴とする密閉形スラスト動圧軸受。

【請求項3】 請求項1または2に記載の密閉形スラスト動圧軸受において、上記フランジの端面に対向するハウジングの受面に、上記環状領域に少なくとも部分的に対向あるいは重なる油溜まりを備えていることを特徴とする密閉形スラスト動圧軸受。

【発明の詳細な説明】

【0001】

【発明の属する技術分野】本発明は、密閉形スラスト動圧軸受に関する。

【0002】

【従来の技術】従来、密閉形スラスト動圧軸受としては、軸体とこの軸体の一端に設けられたフランジとから成る回転体と、この回転体のフランジを密閉状態で収納するハウジングとを備え、上記フランジの軸方向両端面に動圧発生溝を設けたものがある。

【0003】

【発明が解決しようとする課題】ところで、上記従来の密閉形スラスト動圧軸受では、上記回転体が鉛直方向に設置された場合、起動前に上記回転体が重力によって下降し、フランジの下側の端面とそれに対向するハウジングの受面は接触した状態あるいは極めて薄い作動流体の膜しか存在しない状態になっている。この状態で、回転体を起動させると、フランジの軸方向両端面で同時にたとえばV字形の動圧発生溝が作動流体をこの溝の半径方向中央に引き込もうとするが、ハウジングがフランジを密閉状態で収納しているため、フランジの上側の端面とハウジングとの間に負圧が発生し、もともと極めて少量しか作動流体が存在しないハウジングの受面とフランジの下側の端面との間に、特に半径方向内側の部分に十分に作動流体を導くことができないという問題があった。そのため、回転体の起動時に、フランジの下側の端面と受面との間に作動流体が不足した状態となって、フランジを支持する動圧を十分に発生させることができず、スラスト動圧軸受としての機能が果たせず、また、フランジの端面等を損傷するという問題があった。

【0004】そこで、本発明の目的は、起動時に軸方向に支持する動圧を十分に発生することができ、端面等を損傷することがない密閉形スラスト動圧軸受を提供することにある。

【0005】

【課題を解決するための手段】上記目的を達成するため、請求項1の密閉形スラスト動圧軸受は、軸体とこの軸体の一端に設けられたフランジとから成る回転体と、この回転体のフランジを密閉状態で収納するハウジングとを備え、上記フランジの端面またはこの端面に対向する上記ハウジングの受面に動圧発生溝が設けられている密閉形スラスト動圧軸受において、上記フランジは、上記動圧発生溝が設けられた環状領域よりも径方向内側に軸方向に貫通する少なくとも1つの孔を備えているを特徴としている。

【0006】請求項1の密閉形スラスト動圧軸受によれば、回転体の軸が鉛直状態で回転体が回転すると、上記フランジの上側の端面とハウジングの受面との間の作動流体が、上記フランジを貫通する孔を通ってフランジの下側の端面とハウジングの受面との間に補給されるので、動圧発生溝に十分な作動流体を供給できる。したがって、フランジの軸方向の支持を行う動圧が十分に発生して、スラスト動圧軸受としての機能を果たすことができ、また、フランジの下側の端面とそれに対向するハウジングの受面とが損傷する事がない。

【0007】請求項2の密閉形スラスト動圧軸受は、請求項1に記載の密閉形スラスト動圧軸受において、上記孔の断面積の総和が上記環状領域の少なくとも1/30であることを特徴としている。

【0008】請求項2の密閉形スラスト動圧軸受では、上記孔の断面積の総和が上記環状領域の少なくとも1/30あるから、所定回転数で十分な作動流体がフランジの下側の端面に供給されて、十分な動圧が生じる。このことは、実験により確かめられた。

【0009】請求項3の密閉形スラスト動圧軸受は、請求項1または2に記載の密閉形スラスト動圧軸受において、上記フランジの端面に対向するハウジングの受面に、上記環状領域に少なくとも部分的に対向あるいは重なる油溜まりを備えていることを特徴としている。

【0010】請求項3の密閉形スラスト動圧軸受によれば、上記フランジの端面に対向するハウジングの受面上に、上記環状領域に少なくとも部分的に対向あるいは重なる油溜まりを備えているから、回転体起動時ににおけるフランジの下側の端面への作動流体の供給はこの油溜まりからも行なわれ、動圧発生溝による動圧の発生がより確実に行なわれる。

【0011】

【発明の実施の形態】以下、本発明を図示の実施の形態により詳細に説明する。

50 【0012】図1(a)は、本発明の一実施の形態の断面

図である。但し、ハウジング2については、見やすくするために、ハッキングを省略している。

【0013】図1(a)に示すように、回転体3は軸体4とその端に固定したフランジ1から成る。上記軸体4およびフランジ1はハウジング2によってラジアルおよびアキシャル方向に支持している。上記フランジ1はハウジング2内に密封状態に収容している。上記フランジ1の上下両側の端面5,6には、図1(a),(b)に示すように、環状領域7にV字形の動圧発生溝8を設けている。この環状領域7は、図1(b)では、円9と円10との間の領域である。

【0014】また、上記フランジ1の環状領域7よりも半径方向内側には、8個の貫通孔11を円周上に等間隔で設けている。この貫通孔11の断面積の総和は、環状領域7の面積の1/30以上になっている。

【0015】一方、上記フランジ1の下側の端面6と対向する受面12には、上記環状領域7に部分的に対向する複数の油溜まり13を設けている。この油溜まり13は作動流体14が動圧発生溝側8に出て行きやすいように、半径方向内側が滑らかに湾曲している。

【0016】一方、上記軸体4には動圧発生溝15を設けて、軸体4を動圧によってラジアル方向に支持している。

【0017】上記構成の密閉形スラスト動圧軸受の回転体3が鉛直方向に設置された場合、起動前には上記フランジ1は自重によって降下し、フランジ1の下側の端面6とそれに対向するハウジング2の受面12は接触した状態あるいは極めて薄い作動流体14の膜しか存在しない状態になる。この状態で、回転体3を起動させると、V字形の動圧発生溝8が作動流体14をこの溝8の半径方向中央に引き込もうとする。このとき、環状領域7よりも径方向内側においてフランジ1を貫通する孔11によって、フランジ1の上側の端面5とハウジング2の受面12との間の空間と、フランジ1の下側の端面6とハウジング2の受面12との間の空間とが連通している。そのため、作動流体14が、上記孔11を通って図1(a)の矢印E,Fが示すように流れ、フランジ1の下側の端面6とハウジング2の受面12との間に作動流体14が補給される。このため、ハウジング2がフランジ1を密閉状態で収納していても、フランジ1の上側の端面8とハウジング2との間に負圧が発生しない。このため、ハウジング2の受面12とフランジ1の下側の端面6との間に、矢印D,E,Fに示すように、特に半径方向内側の部分に十分に作動流体14を補給して、起動時から動圧を発生させることができる。

【0018】このように、回転体3の起動時に、フランジ1の下側の端面6の環状領域7に作動流体14が十分に補給されるので、動圧発生溝8の設けられた環状領域7にフランジ1を軸方向に支持する動圧を十分に発生させることができ、スラスト動圧軸受としての機能を果たす

ことができる。

【0019】また、上記油溜まり13から、フランジ1の動圧発生溝8は、作動流体14を引っ張り込む。すなわち、フランジ1の回転時に、上記動圧発生溝8が動圧発生溝8直下の油溜まり13から作動流体14を引っ張り込むので、上記油溜まり13がない場合に比較して、作動流体14はフランジ1の下側の端面6とハウジング2の受面12との間に一層容易に補給される。

【0020】図2は作動流体14を循環させるための全ての孔11の面積の総和と環状領域7の面積との比に対する回転体3の浮上量の関係を示す。詳しくは、図2は回転体3の回転数を1000r.p.m., 3000r.p.m., 5000r.p.m.と変化させた場合に、作動流体14用の全ての孔11の総面積と環状領域7の面積との比に対する回転体3の浮上量の関係を示す図である。上記孔11の総面積と環状領域7の面積との比が1/30以上であれば、回転体3の回転数が1000r.p.m., 3000r.p.m., 5000r.p.m.と変化した場合、回転体3の浮上量は、それぞれ約5μm, 5.5μm, 6μmとなって設定浮上量5μm以上になる。したがって、フランジ1を貫通する作動流体14用の孔11の面積の総和と環状領域7の面積に対する比が1/30以上であり、回転体3の回転数が1000r.p.m.以上であると、回転体3は設定浮上量である5μm以上を確保することができる。

【0021】なお、上記実施の形態では、動圧発生溝8はフランジ1の上下側の端面5,6に設けられているが、動圧発生溝を上記端面に対向するハウジングの受面に設けてよい。

【0022】また、油溜まりは、図示しないが、このフランジの端面に設けてよい。この油溜まりは、動圧発生溝のある環状領域に對向するようにしてもよいし、あるいは、この環状領域に部分的に重なってもよい。また、実施の形態では、油溜まり13はハウジング2の受面12の外周部分に複数設けられているが、ハウジング受面の内周部分に設けてよい。また、油溜まりの形状は、丸穴、円弧形あるいはリング形であってもよい。

【0023】

【発明の効果】以上より明らかなように、請求項1の動圧軸受は、軸体とこの軸体の一端に設けられたフランジとから成る回転体と、この回転体のフランジを密閉状態で収納するハウジングとを備え、上記フランジの端面またはこの端面に對向する上記ハウジングの受面に動圧発生溝が設けられている密閉形スラスト動圧軸受において、上記フランジは、上記動圧発生溝が設けられた環状領域よりも径方向内側に軸方向に貫通する少なくとも1つの孔を備えているので、この孔を通して上記フランジの下側の端面とこの面に對向する上記ハウジングの面との間に作動流体を十分に補給できる。したがって、フランジの軸方向の支持を行う動圧を十分に発生させて、起動時にスラスト動圧軸受としての機能を果たすことがで

き、フランジの端面とハウジングの受面の損傷を防止できる。

【0024】また、請求項2の動圧軸受は、請求項1に記載の動圧軸受において、上記孔の断面積の総和が環状領域の面積の少なくとも $1/30$ であるので、フランジの下側の端面とこの面に対向する上記ハウジングの面との間に作動流体を十分に補給でき、設定浮上量を確保することができる。

【0025】また、請求項3の動圧軸受は、請求項1に記載の動圧軸受において、上記フランジの端面に対向するハウジングの受面に、上記環状領域に少なくとも部分的に対向あるいは重なる油溜まりを備えているので、上記フランジの下側の端面とこの面に対向する上記ハウジ*

*ングの面との間に作動流体をより確実に補給できる。

【図面の簡単な説明】

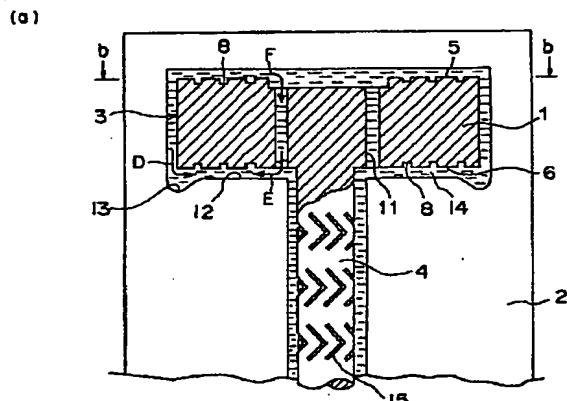
【図1】 図1(a)は本発明の一実施の形態に係る動圧軸受の断面図である。図1(b)は、フランジの上側の端面の平面図である。

【図2】 図2は孔の総面積と環状領域との比に対する回転体の浮上量を示す。

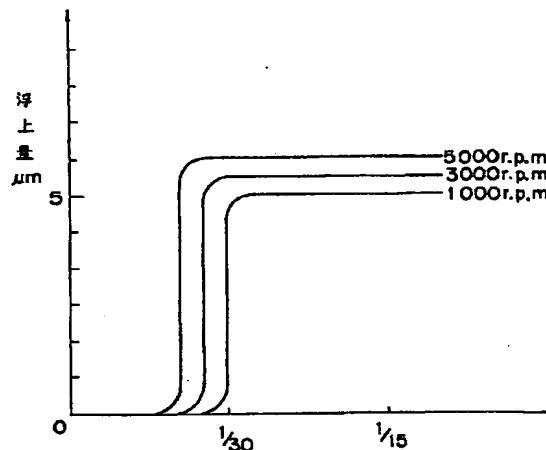
【符号の説明】

1…フランジ、 2…ハウジング、 3…回転体、 4…軸体、 5…フランジの上側の端面、 6…フランジの下側の端面、 7…環状領域、 8…動圧発生溝、 11…孔、 12…ハウジングの受面、 13…油溜まり。

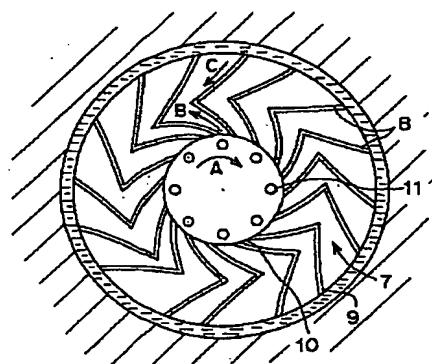
【図1】



【図2】



(b)



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Bibliography

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(54) [Title of the Invention] Sealing form thrust hydrodynamic bearing
(51) [International Patent Classification (6th Edition)]

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[The number of claims] 3
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(71) [Applicant]
[Identification Number] 000001247
[Name] Koyo Seiko Co., Ltd.
[Address] 3-5-8, Minami-senba, Chuo-ku, Osaka-shi, Osaka
(72) [Inventor(s)]
[Name] Takahashi **
[Address] 3-5-8, Minami-senba, Chuo-ku, Osaka-shi, Osaka Inside of Koyo Seiko Co., Ltd.
(74) [Attorney]
[Patent Attorney]
[Name] Aoyama ** (besides one person)

[Translation done.]

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Epitome

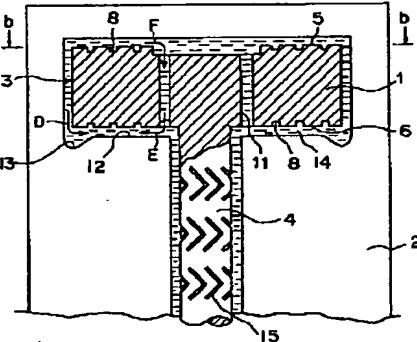
(57) [Abstract]

[Technical problem] The dynamic pressure supported to shaft orientations at the time of starting can fully be generated, and the sealing form thrust hydrodynamic bearing which does not damage an end face etc. is offered.

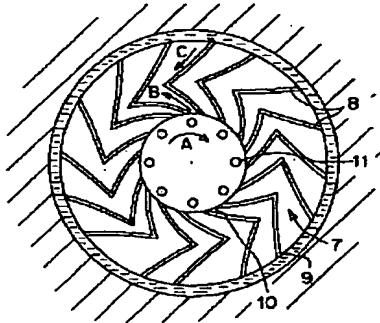
[Means for Solution] The flange 1 of body of revolution 3 is contained in the state of seal in housing 2. While establishing the dynamic pressure generating slot 8 of V typeface in the vertical both-ends sides 5 and 6 of the above-mentioned flange 1, two or more holes 11 penetrated to shaft orientations at the direction inside of a path are formed in the above-mentioned flange 1 from the dynamic pressure generating slot 8. Moreover, total of the cross section of the above-mentioned hole 11 may be 1/30, even if there is little ring domain 7 area. Furthermore, the sump ball 13 is formed in the abutment 12 of the housing 2 which counters the end face 6 of the above-mentioned flange 1 bottom.

[Translation done.]

(a)



(b)



[Translation done.]

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CLAIMS

[Claim(s)]

[Claim 1] It has the body of revolution which consists of the flange prepared in the end of an axis and this axis, and housing which contains the flange of this body of revolution in the state of sealing. In the sealing form thrust hydrodynamic bearing by which the dynamic pressure generating slot is established in the abutment of the above-mentioned housing which counters the end face or this end face of the above-mentioned flange the above-mentioned flange The sealing form thrust hydrodynamic bearing characterized by having at least one hole penetrated to shaft orientations at the direction inside of a path rather than the ring domain in which the above-mentioned dynamic pressure generating slot was established.

[Claim 2] The sealing form thrust hydrodynamic bearing to which total of the cross section of the above-mentioned hole is characterized by being [of the above-mentioned ring domain] 1/30 at least in a sealing form thrust hydrodynamic bearing according to claim 1.

[Claim 3] The sealing form thrust hydrodynamic bearing characterized by equipping partially at least the abutment of housing which counters the end face of the above-mentioned flange with opposite or the lapping sump ball in the above-mentioned ring domain in a sealing form thrust hydrodynamic bearing according to claim 1 or 2.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention relates to a sealing form thrust hydrodynamic bearing.

[0002]

[Description of the Prior Art] Conventionally, it has the body of revolution which consists of the flange prepared in the end of an axis and this axis as a sealing form thrust hydrodynamic bearing, and housing which contains the flange of this body of revolution in the state of sealing, and there are some which established the dynamic pressure generating slot in the shaft-orientations both-ends side of the above-mentioned flange.

[0003]

[Problem(s) to be Solved by the Invention] By the way, in the above-mentioned conventional sealing form thrust hydrodynamic bearing, when the above-mentioned body of revolution is installed in the direction of a vertical, the above-mentioned body of revolution descends with gravity before starting, and the end face of the flange bottom and the abutment of housing which counters it are in the condition that only the film of the condition which contacted, or a very thin working fluid exists. Although the dynamic pressure generating slot of for example, V typeface tends to draw a working fluid in coincidence in the center of radial of this slot in respect of the shaft-orientations both ends of a flange in this condition if body of revolution is started Since housing has contained the flange in the state of sealing, between the abutment of housing with which negative pressure occurs between the end face of a flange top, and housing, and a little deer working fluid does not exist in it extremely from the first, and the end face of the flange bottom There was a problem that a working fluid could not fully be led especially to the part of the radial inside. Therefore, there was a problem of being in the condition that working fluids ran short between the end face of the flange bottom and the abutment, could not fully generate

the dynamic pressure which supports a flange, and could not achieve the function as a thrust hydrodynamic bearing, and damaging the end face of a flange etc. at the time of starting of body of revolution.

[0004] Then, the purpose of this invention is to offer the sealing form thrust hydrodynamic bearing which can fully generate the dynamic pressure supported to shaft orientations, and does not damage an end face etc. at the time of starting.

[0005]

[Means for Solving the Problem] In order to attain the above-mentioned purpose, the sealing form thrust hydrodynamic bearing of claim 1 It has the body of revolution which consists of the flange prepared in the end of an axis and this axis, and housing which contains the flange of this body of revolution in the state of sealing. In the sealing form thrust hydrodynamic bearing by which the dynamic pressure generating slot is established in the abutment of the above-mentioned housing which counters the end face or this end face of the above-mentioned flange the above-mentioned flange Rather than the ring domain in which the above-mentioned dynamic pressure generating slot was established, the direction inside of a path is equipped with at least one hole penetrated to shaft orientations, and it is characterized by **.

[0006] According to the sealing form thrust hydrodynamic bearing of claim 1, since the shaft of body of revolution is supplied between the end face of the flange bottom, and the abutment of housing through the hole with which the working fluid between the end face of the above-mentioned flange top and the abutment of housing will penetrate the above-mentioned flange if body of revolution rotates in the state of a vertical, enough working fluids for a dynamic pressure generating slot can be supplied. Therefore, the dynamic pressure which supports the shaft orientations of a flange fully occurs, and the function as a thrust hydrodynamic bearing can be achieved, and the end face of the flange bottom and the abutment of housing which counters it are not damaged.

[0007] In the sealing form thrust hydrodynamic bearing according to claim 1, as for the sealing form thrust hydrodynamic bearing of claim 2, total of the cross section of the above-mentioned hole is characterized by being [of the above-mentioned ring domain] 1/30 at least.

[0008] In the sealing form thrust hydrodynamic bearing of claim 2, since total of the cross section of the above-mentioned hole has the above-mentioned ring domain 1/30 at least, working fluids enough at a predetermined engine speed are supplied to the end face of the flange bottom, and sufficient dynamic pressure arises. This was confirmed by the experiment.

[0009] The sealing form thrust hydrodynamic bearing of claim 3 is characterized by equipping partially at least the abutment of housing which counters the end face of the above-mentioned flange with opposite or the lapping sump ball in the above-mentioned ring domain in the sealing form thrust hydrodynamic bearing according to claim 1 or 2.

[0010] According to the sealing form thrust hydrodynamic bearing of claim 3, since the abutment of housing which counters the end face of the above-mentioned flange is partially equipped with opposite or the lapping sump ball at least in the above-mentioned ring domain, supply of the working fluid to the end face of the flange bottom at the time of body-of-revolution starting is performed also from this sump ball, and generating of the dynamic pressure by the dynamic pressure generating slot is ensured.

[0011]

[Embodiment of the Invention] Hereafter, the gestalt of implementation of illustration explains this invention to a detail.

[0012] Drawing 1 (a) is the sectional view of the gestalt of 1 operation of this invention. However, about housing 2, in order to make it legible, hatching is omitted.

[0013] As shown in drawing 1 (a), body of revolution 3 consists of the flange 1 fixed to an axis 4 and its edge. The above-mentioned axis 4 and the flange 1 are supported in a radial and the axial direction with housing 2. The above-mentioned flange 1 is held in housing 2 at the seal condition. As shown in the end faces 5 and 6 of the vertical both sides of the above-mentioned flange 1 at drawing 1 (a) and (b), the dynamic pressure generating slot 8 of V typeface is established in the ring domain 7. This ring domain 7 is a field between a circle 9 and a circle 10 in drawing 1 (b).

[0014] Moreover, eight through tubes 11 are formed at equal intervals on the periphery rather than the ring domain 7 of the above-mentioned flange 1 at the radial inside. Total of the cross section of this through tube 11 has become 1/30 or more [of the area of a ring domain 7].

[0015] On the other hand, two or more sump balls 13 which counter the above-mentioned ring domain 7 partially are formed in the end face 6 of the above-mentioned flange 1 bottom, and the abutment 12 which counters. The

radial inside is curving smoothly so that a working fluid 14 may tend to leave this sump ball 13 in dynamic pressure generating slot side 8.

[0016] On the other hand, the dynamic pressure generating slot 15 is established in the above-mentioned axis 4, and the axis 4 is supported to the radial direction with dynamic pressure.

[0017] When the body of revolution 3 of the sealing form thrust hydrodynamic bearing of the above-mentioned configuration is installed in the direction of a vertical, before starting, the above-mentioned flange 1 descends with a self-weight, and the end face 6 of the flange 1 bottom and the abutment 12 of the housing 2 which counters it will be in the condition that only the film of the condition which contacted, or the very thin working fluid 14 exists. In this condition, if body of revolution 3 is started, the dynamic pressure generating slot 8 of V typeface tends to draw a working fluid 14 in the center of radial of this slot 8. At this time, the space between the end face 5 of a flange 1 top and the abutment 12 of housing 2 and the space between the end face 6 of the flange 1 bottom and the abutment 12 of housing 2 are open for free passage with the hole 11 which penetrates a flange 1 in the direction inside of a path rather than a ring domain 7. Therefore, a working fluid 14 flows, as the arrow heads E and F of drawing 1 (a) show through the above-mentioned hole 11, and a working fluid 14 is supplied between the end face 6 of the flange 1 bottom, and the abutment 12 of housing 2. For this reason, even if housing 2 has contained the flange 1 in the state of sealing, negative pressure does not occur between the end face 8 of a flange 1 top, and housing 2. For this reason, between the abutment 12 of housing 2, and the end face 6 of the flange 1 bottom, as shown in arrow heads D, E, and F, a working fluid 14 can fully be supplied to especially the part of the radial inside, and dynamic pressure can be generated from the time of starting.

[0018] Thus, since a working fluid 14 is fully supplied to the ring domain 7 of the end face 6 of the flange 1 bottom at the time of starting of body of revolution 3, the dynamic pressure which the dynamic pressure generating slot 8 prepares and supports a flange 1 to shaft orientations in the **** ring domain 7 can fully be generated, and the function as a thrust hydrodynamic bearing can be achieved.

[0019] Moreover, the dynamic pressure generating slot 6 of a flange 1 brings in a working fluid 14 from the above-mentioned sump ball 13. That is, at the time of rotation of a flange 1, since the above-mentioned dynamic pressure generating slot 8 brings in a working fluid 14 from the sump ball 13 of dynamic pressure generating slot 8 directly under, as compared with the case where there is no above-mentioned sump ball 13, a working fluid 14 is supplied still more easily between the end face 6 of the flange 1 bottom, and the abutment 12 of housing 2.

[0020] Drawing 2 shows the relation of the flying height of body of revolution 3 to the ratio of total of the area of all the holes 11 for circulating a working fluid 14, and the area of a ring domain 7. In detail, drawing 2 is drawing showing the relation of the flying height of body of revolution 3 to the ratio of the gross area of all the holes 11 for working-fluid 14, and the area of a ring domain 7, when changing the rotational frequency of body of revolution 3 with 1000r.p.m., 3000r.p.m., and 5000r.p.m. When the ratio of the gross area of the above-mentioned hole 11 and the area of a ring domain 7 was 1/30 or more and the rotational frequency of body of revolution 3 changes with 1000r.p.m., 3000r.p.m., and 5000r.p.m., the flying height of body of revolution 3 is set to about 5 micrometers, 5.5 micrometers, and 6 micrometers, respectively, and turns into 5 micrometers or more of setting flying heights. Therefore, the ratio to the total of the area of the hole 11 for working-fluid 14 and the area of a ring domain 7 which penetrate a flange 1 is 1/30 or more, and 5 micrometers or more whose body of revolution 3 is the setting flying height as the rotational frequency of body of revolution 3 is more than 1000r.p.m. can be secured.

[0021] In addition, with the gestalt of the above-mentioned implementation, although the dynamic pressure generating slot 8 is established in the end faces 5 and 6 by the side of the upper and lower sides of a flange 1, it may establish a dynamic pressure generating slot in the abutment of housing which counters the above-mentioned end face.

[0022] Moreover, although a sump ball is not illustrated, it may be formed in the end face of this flange. You may make it this sump ball counter a ring domain with a dynamic pressure generating slot, or it may lap with this ring domain partially. Moreover, with the gestalt of operation, although two or more sump balls 13 are formed in the periphery part of the abutment 12 of housing 2, they may be formed in the inner circumference part of a housing abutment. Moreover, the configuration of a sump ball may be a round hole, a radii form, or a ring form.

[0023]

[Effect of the Invention] So that clearly as mentioned above, the hydrodynamic bearing of claim 1 It has the body of revolution which consists of the flange prepared in the end of an axis and this axis, and housing which contains the flange of this body of revolution in the state of sealing. In the sealing form thrust hydrodynamic bearing by which the dynamic pressure generating slot is established in the abutment of the above-mentioned

housing which counters the end face or this end face of the above-mentioned flange the above-mentioned flange Since the direction inside of a path is equipped with at least one hole penetrated to shaft orientations rather than the ring domain in which the above-mentioned dynamic pressure generating slot was established, a working fluid can fully be supplied through this hole between the end face of the above-mentioned flange bottom, and the field of the above-mentioned housing which counters this field. Therefore, the dynamic pressure which supports the shaft orientations of a flange can fully be generated, the function as a thrust hydrodynamic bearing can be achieved at the time of starting, and damage on the end face of a flange and the abutment of housing can be prevented.

[0024] Moreover, in a hydrodynamic bearing according to claim 1, since the area of a ring domain is 1/30 at least, total of the cross-sectional area of the above-mentioned hole can fully supply a working fluid between the end face of the flange bottom, and the field of the above-mentioned housing which counters this field, and the hydrodynamic bearing of claim 2 can secure the setting flying height.

[0025] Moreover, in a hydrodynamic bearing according to claim 1, since the hydrodynamic bearing of claim 3 equips the above-mentioned ring domain with opposite or the lapping sump ball partially at least in the abutment of housing which counters the end face of the above-mentioned flange, it can supply a working fluid more certainly between the end face of the above-mentioned flange bottom, and the field of the above-mentioned housing which counters in this field.

[Translation done.]

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] Drawing 1 (a) is the sectional view of the hydrodynamic bearing concerning the gestalt of 1 operation of this invention. Drawing 1 (b) is the top view of the end face of a flange top.

[Drawing 2] Drawing 2 shows the flying height of body of revolution to the ratio of the gross area of a hole, and a ring domain.

[Description of Notations]

- 1 — Flange 2 — Housing 3 — Body of revolution 4 [6 — End face of the flange bottom 7 — Ring domain,] — An axis, 5 — End face of a flange top
8 — Dynamic pressure generating slot 11 — Hole 12 — The abutment of housing, 13 — Sump ball.

[Translation done.]

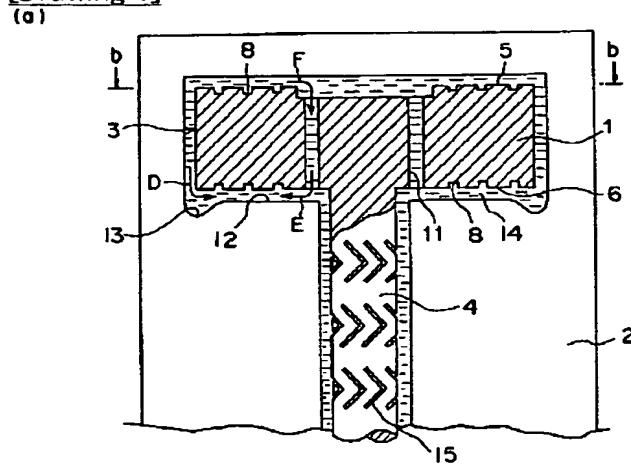
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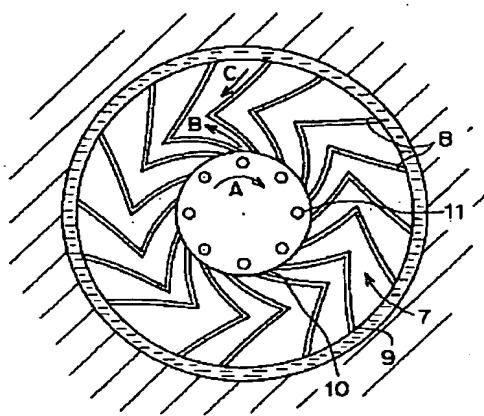
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DRAWINGS

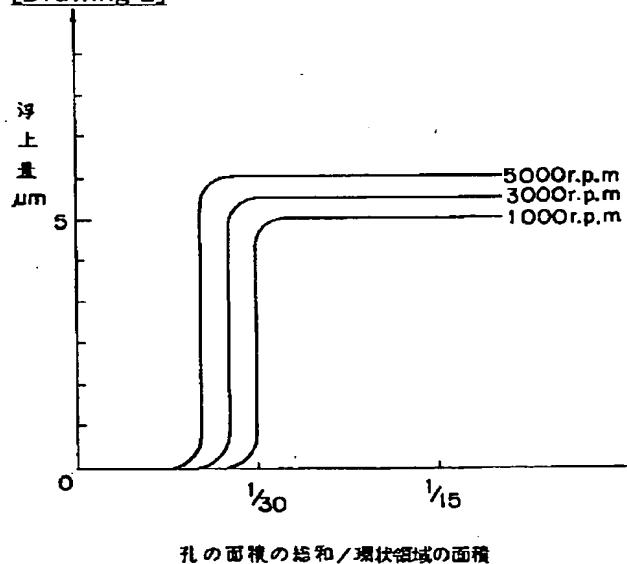
[Drawing 1]



(b)



[Drawing 2]



[Translation done.]